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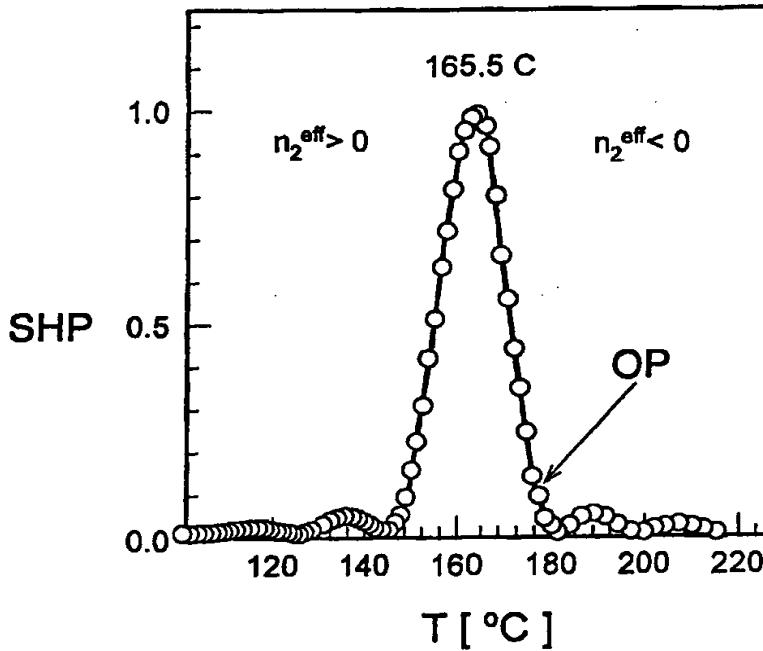
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(54) Title: NON-LINEARITY COMPENSATION IN OPTICAL DEVICES AND TRANSMISSION SYSTEMS

(57) Abstract

A method of and apparatus for compensating optical non-linearity in optical devices and transmission systems. Two second order interactions are cascaded in phase-mismatched second harmonic generation to accumulate a non-linear phase shift of a fundamental wave. The non-linear phase shift can be set to provide a desired amount of non-linearity compensation. Compensation takes place in a compensating medium having a negative effective non-linear refractive index at the design operating conditions of the compensating medium. Compensators incorporating these principles may be incorporated as passive or active components in optical transmitters, repeaters or receivers. Active components may be tuned by varying the operating condition of the compensating medium, for example by controlling temperature or applied stress. Embodiments of the invention use the compensator as pre- or post-compensators in an optical amplifier, to eliminate or reduce self-phase modulation in the optical amplifier that occurs as a result of the Kerr effect.



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TITLE OF THE INVENTION**NON-LINEARITY COMPENSATION IN OPTICAL DEVICES AND
TRANSMISSION SYSTEMS**

5

BACKGROUND OF THE INVENTION

The invention relates to compensation of optical non-linearities in optical devices and transmission systems, more especially, but not exclusively, to compensating for optical non-linearities that occur during optical amplification.

The unquestionable need for ultra-high bit rate transmission systems dictates the development of optical amplifiers of new generation capable of handling of picosecond optical pulses over the entire range of the third optical window. So far the main activity in this area has been concentrated on development of efficient amplifiers with low noise figures, flat gain curves and ultra-broad bandwidths (see, for example [1,2]).

However one topic has not been addressed adequately, namely the nonlinear distortion of Kerr non-linearity which can occur during pulse amplification in an optical amplifier.

20 The main impact of the Kerr non-linearity on transmission carriers is the effect of self-phase modulation (SPM) which results in spectral enrichment of the propagating pulses, i.e. degradation of the pulse from a signal transmission standpoint.

25 As is well known, the refractive index of any material consists of linear and nonlinear parts. On a fundamental level, the origin of the nonlinear response is related to the anharmonic motion of bound electrons under the applied field. Thus, the induced polarization P becomes a non-linear function of the applied field E and may be written as:

$$P = \epsilon_0 (\chi^{(1)} \cdot E + \chi^{(2)} : EE + \chi^{(3)} : EEE), \quad (1)$$

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where ϵ_0 is the vacuum permittivity and $\chi^{(i)}$ is the i-th order susceptibility. The linear susceptibility $\chi^{(1)}$ represents the main contribution to P . Its effects are included through the refractive index and attenuation coefficient. The second-order susceptibility accounts for second harmonic (SH) and sum-frequency generation which 5 normally do not exist in optical fibers.

The lowest-order non-linearity in optical fibers originates from the third-order non-linearity and results in self-phase modulation (SPM), third-harmonic generation, four-wave mixing, and Raman and Brillouin scattering.

10 The existence of $\chi^{(3)}$ means that the medium (i.e. glass) has a refractive index which is proportional to the optical intensity $|E|^2$ and this otherwise small effect becomes noticeable at high illumination. Under intense illumination the refractive index can be represented as:

$$n(\omega, |E|^2) = n(\omega) + n_2 |E|^2 \quad (2)$$

15 where $n(\omega)$ is the linear part and n_2 is the non-linear coefficient related to $\chi^{(3)}$ by the expression:

$$n_2 = \frac{3}{8n} \operatorname{Re}(\chi^{(3)}) \quad (3)$$

20 Here Re represents the real part and the optical field is assumed to be linearly polarized. In practice, however, very often the polarization is completely scrambled which reduces the effective non-linear refractive index. In silica n_2 is dominated by the electronic contribution, so to a good approximation the following expression holds (see [3]):

25

$$(n_2 |E|^2)_{\text{average}} = \frac{5}{6} (n_2 |E|^2)_{\text{linear}} \quad (4)$$

The intensity-dependent refractive index leads to an intensity-dependent phase of the propagating wave, i.e.

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$$\phi(t, |E|^2) = knz = k(n_0 + n_2 |E|^2)z = \phi_{lin} + \phi_{nl} \quad (5)$$

where $k=2\pi/\lambda$ is the wave-number. In practical computations it is more convenient to use light intensity rather than electrical fields so that Equation (5) may be written in
5 the form

$$\phi_{nl} = kn_2 I z \quad (6)$$

and we can define a nonlinear length z_{nl} as

10

$$\phi_{nl} = kn_2 I z_{nl} = 1 \quad (7)$$

or

$$z_{nl} = (kn_2 I)^{-1} \quad (8)$$

15

where I is the light intensity in W/cm^2 and $n_2 = 2.6 \cdot 10^{-16} \text{cm}^2/\text{W}$. Such a small value of the non-linear refractive index causes negligible changes in the value of the refractive index itself (even pulses with 100 kW peak power result in $\sim 4 \cdot 10^{-5}$ refractive index change which is approximately two orders of magnitude lower than the core-cladding
20 refractive index difference).

The main effect caused by the non-linear refractive index is the generation of new spectral components due to self-phase modulation (SPM) i.e. spectral enrichment of the propagating pulses. This is because the non-linear phase given by Equation (6) incurs a time-dependent variation of the instantaneous frequency ω that can be written

25 as

$$\omega = \omega_0 + \frac{\partial \phi_{nl}}{\partial t} = \omega_0 + kn_2 z \frac{\partial I}{\partial z} \quad (9)$$

or

$$\omega - \omega_0 = kn_z z \frac{\partial I}{\partial t} \quad (10)$$

Thus the shorter the pulses and the higher their intensity the greater the spectral enrichment due to SPM. The most interesting and important consequence of SPM is 5 not spectral broadening itself but nonlinear interaction of the spectral components in a pulse due to group velocity dispersion.

Figure 1A of the accompanying drawings shows an intensity profile of an optical pulse, as a function of time in arbitrary units, propagating down an optical fiber. SPM will tend to result in a frequency distribution of the pulse as illustrated in 10 Figure 1B of the accompanying drawings.

Figure 1B illustrates how the lower frequency components of the pulse are gathered on the leading edge of the pulse, while higher frequency components of the pulse are mainly gathered at the trailing edge.

Spectral broadening results not only in temporal broadening due to chromatic 15 dispersion, but also causes additional noise. SPM is proportional to the pulse intensity and the active length of the gain or amplification element, e.g. length of an erbium doped fiber amplifier (EDFA).

An obvious way to cope with SPM is to reduce either the pulse intensity or active length or both. For example, Richardson et al suggested the use of large mode 20 area fibers [4] and Fermann [5] demonstrated advantages of selective excitation of multimode fibers.

However these approaches do not solve the problem of non-linearity, but merely avoid operating conditions in which the non-linearities occur in the amplifier element. The fundamental inherent problem of the non-linearities is thus not addressed by these 25 prior art approaches. Neither of the suggested approaches is attractive, since in both cases gain and launch intensity must be limited, whereas high gain and/or high launch intensity are generally desirable.

SUMMARY OF THE INVENTION

We suggest a radical approach to the problem. Namely, instead of minimizing SPM, we compensate SPM by exploiting a second order cascading non-linearity.

5 Cascading of two second order interactions in phase-mismatched second harmonic generation (SHG) results in accumulation of a nonlinear phase shift of the fundamental wave.

10 This phenomenon was predicted in the late 1960's. Using efficient high power sources this effect was studied further in the early 1990's, when high nonlinear phase shifts in quadratic media were experimentally demonstrated [6].

15 According to one aspect of the invention there is provided a method of compensating optical non-linearity comprising cascading two second order interactions in phase-mismatched second harmonic generation to accumulate a non-linear phase shift of a fundamental wave.

20 According to another aspect of the invention there is provided a method of compensating optical non-linearity by providing a compensating medium having a negative effective non-linear refractive index at an operating condition of the compensating medium.

25 According to a further aspect of the invention there is provided a non-linearity compensator having a design operating condition and comprising a compensating medium having a negative effective non-linear refractive index at the design operating condition.

30 The non-linearity compensator may form part of a transmitter, repeater or receiver, either as a pre-compensator or post-compensator. For optical fiber dispersion compensation, pre-compensation is preferable in view of the fact that a pre-compensator can be kept sufficiently short that the role of dispersion is effectively negligible.

According to another aspect of the invention there is provided an optical device having an active medium with an intensity dependent refractive index component and a compensating medium with an effective non-linear refractive index component which is also intensity dependent.

5 The effective non-linear refractive index component of the device is operating condition dependent and the respective refractive index components of the media may be tailored to partially or wholly cancel each other at a particular operating condition of the optical device. Generally, the operating condition defines the phase mismatch between fundamental and second harmonic waves in the compensating medium, which in turn sets the amount of compensation through the value of the intensity dependent refractive index component of the compensating medium.

10 The active medium may be a gain medium. In some embodiments of the invention, the optical device is an optical amplifier.

15 The active medium may be arranged prior to the compensating medium which serves as a post-compensator. Alternatively, the active medium may be arranged after to the compensating medium which serves as a pre-compensator. In another alternative, the active medium and the compensating medium may be the same medium.

20 The compensating medium may be periodically poled.

25 According to a further aspect of the invention there is provided an optical amplifier comprising: means for launching optical signal into an optical amplifier, the instantaneous frequency of the input signal varying with intensity so that leading edge of the pulses is enriched with higher (in respect to central wavelength) frequencies whereas the lower spectral frequencies situated mainly at the trailing edge of the pulse; launching pre-compensated optical pulses into optical amplifier exhibiting nonlinear behavior.

30 The high intensity optical pulses may cause increase of refractive index of an optical amplifier

25 The pulse intensity may be between 1 W/cm² and 10¹² W/cm².

The non-linearity of the optical amplifier may be Kerr non-linearity.

35 The optical amplifier may be a fiber amplifier, for example based on a silica fiber. Alternatively, the optical amplifier may be a planar amplifier, for example based on LiNbO₃ or a silica planar amplifier.

40 If a fiber amplifier is used, the fiber may be doped in various ways, for example doped with Er, Nd, Pr, Yb, Tm, Ho; co-doped with Er/Yb; and/or doped with germanium, phosphorous, boron, aluminum or fluoride.

The fiber of any such fiber amplifier may be periodically poled fiber with effective second order non-linearity greater than 0.01 pm/V. The periodically poled fiber may be doped with Er, Nd, Pr, Yb, Tm, Ho.

In the case of a planar amplifier, this may be a LiNbO₃ planar amplifier that is 5 periodically poled.

The amplifier gain may be less than 1. The amplifier length may be between 1mm and 1km, or between 1 km and 100 km.

Viewed from another aspect the invention provides an optical amplifier having 10 non-linear behavior and a pre-compensator for pre-compensating optical pulses to be passed to said optical amplifier so as to counteract said non-linear behavior of said optical amplifier.

BRIEF DESCRIPTION OF THE DRAWINGS

For a better understanding of the invention and to show how the same may be carried into effect reference is now made by way of example to the accompanying drawings in which:

Figure 1A shows pulse intensity as a function of time in arbitrary units for an optical pulse;

Figure 1B shows, for the pulse of Figure 1A, pulse instantaneous frequency as a function of time in arbitrary units;

Figure 2 shows the variation of second harmonic power (SHP) generated in a crystal as a function of temperature of the crystal;

Figure 3 shows a first embodiment of the invention which comprises an optical amplifier with a non-linearity pre-compensator;

Figure 4A is a spectrum of a pulse received at the input of an EDFA;

Figure 4B is a spectrum of a pulse transmitted from the output of the EDFA without non-linearity compensation (prior art performance);

Figure 4C is a spectrum of a pulse transmitted from the output of the EDFA with non-linearity compensation (performance of first embodiment);

Figure 5 shows a second embodiment of the invention including an attenuator arranged between the non-linearity pre-compensator and the optical amplifier;

Figure 6 shows a third embodiment of the invention including an optical amplifier and non-linearity post-compensator; and

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Figure 7 shows a fourth embodiment of the invention including a non-linearity compensator acting as a passive component arranged as an input stage of a repeater station.

DETAILED DESCRIPTION**Principles of the Invention**

5 As stated above, the invention is based on exploiting a second order cascading non-linearity. The cascading effect arises when the phase-matched condition is not satisfied, i.e. $\Delta k = k_{2\omega} - 2k_{\omega} \neq 0$. In this circumstances, the second harmonic (SH) field propagates with a phase velocity ($c_0/n_{2\omega}$) different from the phase velocity of the nonlinear polarization that drives it and from that of the fundamental beam (c_0/n_{ω}).
 10 This results in a periodic exchange of power between the two propagating fields, with half a period defined as "coherence length" (l_c).

An "up-conversion" ($\omega \rightarrow 2\omega$) over a coherence length follows a "down-conversion" ($2\omega \rightarrow \omega$), that justifies the name "cascading" given to this phenomenon. After a coherence length, the accumulated phase difference between the fields is such 15 that the energy flow changes sign and the double-frequency field begins to transfer energy to the fundamental. But now the down-converted field has a different phase with the non-converted one and this results in a phase shift of the fundamental wave (as well as of the generated field).

For low SHG conversion efficiency the resulting interaction is similar to the 20 classical Kerr-effect but with an effective nonlinear refractive index n_2^{eff} which depends on the quadratic nonlinear coefficient, and on ΔkL where Δk is the wave-vector mismatch and can be expressed in the form

$$n_2^{\text{eff}} = \frac{4\pi}{c\epsilon_0} \frac{L}{\lambda} \frac{d_{\text{eff}}^2}{n_{2\omega} n_{\omega}^2} \frac{1}{\Delta k L}, \quad (11)$$

25

where d_{eff} is the quadratic nonlinear coefficient.

The practical significance of equation (11) is that Δk , the wave-vector mismatch, can be controllably set or varied to provide any desired effective nonlinear refractive index n_2^{eff} , positive or negative, within a certain tuning range. The sign of 30 the effective refractive index is changed by changing the sign of the phase mismatch.

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The essence of the present invention is utilization of the cascaded non-linearity in such a way that effective nonlinear refractive index given by equation (11) is of negative sign and a magnitude set to equal the real refractive index associated with the self-phased modulation caused by the Kerr non-linearity, or any other non-linear effect that 5 scales proportional to light intensity. A compensator is thus provided which contains an optical transmission medium with a significant quadratic non-linear coefficient d_{eff} in which the size of the cascaded non-linearity is set to cancel out the SPM from the Kerr non-linearity.

In this respect, it is noted that the other parameters of equation (11) are 10 essentially constants for any given system. (For wavelength division multiplexed (WDM) systems, the multiple operating wavelengths will lie within a relatively narrow band $\Delta\lambda$, giving a range of n_2^{eff} values. This range will however be relatively small since $\Delta\lambda/\lambda$ will typically be large).

15 First Embodiment

A first embodiment of the invention is now described with reference to Figures 2 and 3.

Figure 2 is experimental data showing second harmonic power as a function of 20 temperature for a 4 mm long periodically poled bulk lithium niobate (LiNbO₃) crystal (PPLN) with 18.3 μ m pitch. The tuning curve of the crystal shown in Figure 2, indicates that at temperatures higher than 165⁰ C there should be a negative effective nonlinear refractive index n_2^{eff} , with positive values occurring below that temperature.

Figure 3 shows a first embodiment of the invention built to prove the 25 operational principles experimentally. The apparatus shown comprises a light source 8 in the form of a passively mode-locked fiber laser connected to a non-linearity pre-compensator 10 in the form of the above-mentioned 4mm long PPLN crystal with 18.3 μ m pitch. The pre-compensator 10 has an input line 8 connected to the light source 6 and an output line 12 connected to an input of an optical amplifier 20 in the form of a 2 30 m long erbium doped fiber amplifier (EDFA), the output of which is supplied to an output line 22 for further transmission, for example to a long haul transmission fiber.

The apparatus of Figure 3 was tested by supplying a train of picosecond pulses from the passively mode-locked fiber laser 6. The 1.2 ps bandwidth limited pulses were amplified in the EDFA 20.

Figure 4A shows the input pulse shape as measured at the input 8. The input 5 pulses have a clean 2.3 nm wide spectrum.

Figure 4B shows the output pulse shape at line 22 with a prior-art-like set-up in which the non-linearity pre-compensator 10 was removed (set-up not shown). In other words, the input pulses are supplied directly to the optical amplifier 20. As expected, direct amplification of the picosecond pulses in the optical amplifier 20 results in 10 significant spectral broadening of the amplified pulses due to self-phase modulation with maximum phase shift $\sim 2.5 \pi$. Peak power of the pulses at the output of the amplifier was about 1 kW and the amplifier gain was 15 dB.

Figure 4C shows the output pulse shape at line 22 with the set up of Figure 3, namely where, prior to amplification, the pulses pass through the PPLN 10 which is 15 maintained at a temperature somewhat 10 $^{\circ}\text{C}$ higher than that corresponding to the phase matched condition. This operating point (OP) is indicated in Figure 2 with an arrow. Figure 4C shows that the spectrum of the output pulses is almost identical to that of the input pulses shown in Figure 4A, clearly indicating an effective non-linearity-free operation.

20 Thus our experiment has clearly demonstrated what we believe to be the first ever Kerr-non-linearity free EDFA.

The range of potential uses of such amplifiers is very wide and includes telecommunication systems and power amplifiers for generating high intensity pulses for non-linear applications.

25 It should be understood that the use of this technique is not limited to PPLN. Any material with d_{eff} more than about 0.001 pm/V would perform compensation action of a practical amount for typical applications.

In particular, periodically poled optical fibers are most attractive due to 30 possibility to combine both amplification and compensation actions in a single fiber device.

It should be also understood that both actions, compensation and amplification can be executed within the same amplifier device. Indeed, the gain and compensation

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medium may be the same medium, for example a periodically poled optical fiber with rare earth doping for gain.

Further Embodiments

5

Figure 5 illustrates a second embodiment of the invention. The second embodiment differs from the first embodiment through the addition of an attenuator 15 arranged between the pre-compensator 10 and optical amplifier 20. The inclusion of an attenuator with an attenuation factor M allows a shorter length of compensating 10 material to be used, since the intensity of the light passing through the pre-compensator will be M times larger than that traversing the optical amplifier.

This is useful since, generally, the ratio between effective nonlinear refractive index n_2^{eff} and the relevant component of the real refractive index of the optical 15 amplifier material (typically silica) will be about 1000. That is for every 1 meter of length of optical amplifier fiber, approximately 1 millimeter of path length in the compensator material will be needed to cancel the Kerr non-linearity. (Assuming only one pass of the compensator material, path length will equal actual length of the compensator material). However, with the attenuator, only $1/M$ millimeters of 20 compensator length would be needed in the comparable situation to cancel the Kerr non-linearity.

Figure 6 illustrates a third embodiment of the invention in which the compensator 10 is arranged after the optical amplifier 20 as a post-compensator. It will be understood that the nature of the effect being exploited means that the compensator will function when placed before (Figure 3) or after (Figure 6) the non-linear medium that displays the Kerr effect.

Figure 7 illustrates a fourth embodiment of the invention in which the compensator is also arranged as a post-compensator, as in the third embodiment. In the fourth embodiment, the compensator 10 is arranged as an input stage to a repeater 30 station 25 incorporating conventional amplification components 30. The compensator 10 is provided to compensate for a pre-determined amount of Kerr non-linearity occurring upstream in the fiber link 18. In this way, SPM which occurs at the start of a long-haul fiber link where intensity is highest can be compensated for.

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Similarly the compensator may be used as an input stage to a receiver instead of a repeater station. Indeed the compensator can be used as a passive or active component at any point in a transmission system where Kerr non-linearity, or other functionally similar non-linear effects, need to be compensated for.

5 In the above it has been implicitly assumed that the compensator will be a passive device. However, the temperature sensitivity of the cascade effect renders it suitable for active control, optionally with feedback. As a passive compensator, the device will be temperature stabilized. This will not present any additional burden for many applications where strict temperature stabilization is already needed for stable
10 operation of other devices such as semiconductor lasers. In an active compensator, a conventional temperature controller can be used. It will also be understood that the effect is tunable with parameters other than temperature, for example by applying stress to the compensating medium. The size of the stress can be controlled by conventional apparatus. In the case of a solid state compensator this may be with an
15 external pressure cell. In the case of an optical fiber compensator this may be with an expandable core in an optical fiber coil, as used in fiber sensor technology.

Without feedback, temperature control can be used to switch the compensator between different levels of compensation (including zero compensation, i.e. at the peak of the operating curve shown in Figure 2).

20 With feedback, temperature control can be used to tune the compensator for optimum cancellation of the non-linear effects occurring elsewhere in the transmission system. Training data, for example the bit error rate in training data, may be used to provide the necessary feedback, thereby automatically accounting for non-linearities over the whole transmission line. Standard PID temperature controllers may be used
25 for example.

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CLAIMS

1. A method of compensating optical non-linearity comprising cascading two second order interactions in phase-mismatched second harmonic generation to 5 accumulate a non-linear phase shift of a fundamental wave.
2. A method of compensating optical non-linearity by providing a compensating medium having a negative effective non-linear refractive index.
- 10 3. A method according to claim 2, wherein the negative effective non-linear refractive index is set to a target value for compensating a required amount of non-linearity, the target value being defined by an optimum phase mismatch between fundamental and second harmonic waves traversing the compensating medium.
- 15 4. A non-linearity compensator having a compensating medium with a negative effective non-linear refractive index.
- 20 5. A non-linearity compensator according to claim 4, wherein the negative effective non-linear refractive index is defined by a phase mismatch between fundamental and second harmonic waves in the compensating medium at a design wavelength.
- 25 6. A transmitter, repeater or receiver comprising a non-linearity compensator according to claim 4 or 5.
7. An optical device having an active medium with an intensity dependent refractive index component and a compensating medium with an effective non-linear refractive index component which is also intensity dependent.
- 30 8. An optical device according to claim 7, wherein the respective refractive index components of the media partially or wholly cancel each other at an operating condition of the optical device.

9. An optical device according to claim 8, wherein the operating condition is defined by an operating temperature of the compensating medium.
- 5 10. An optical device according to claim 8 or 9, wherein the operating condition is defined by a stress condition of the compensating medium.
11. An optical device according to any one of claims 7 to 10, wherein the active medium is a gain medium.
- 10 12. An optical device according to claim 11, wherein the optical device is an optical amplifier.
13. An optical device according to any one of claims 7 to 12, wherein the active medium is arranged prior to the compensating medium which serves as a post-compensator.
- 15 14. An optical device according to any one of claims 7 to 12, wherein the active medium is arranged after to the compensating medium which serves as a pre-compensator.
- 20 15. An optical device according to any one of claims 7 to 12, wherein the active medium and the compensating medium are the same medium.
- 25 16. An optical device according to any one of claims 7 to 15, wherein the effective non-linear refractive index component is defined by a phase mismatch between fundamental and second harmonic waves in the compensating medium at a design wavelength.
- 30 17. An optical device according to any one of claims 7 to 16, wherein the compensating medium is periodically poled.

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18. An optical device according to any one of claims 7 to 17, wherein the compensating medium is optical fiber.
19. An optical device according to any one of claims 7 to 18, wherein the active
5 medium is optical fiber.

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Fig. 1A

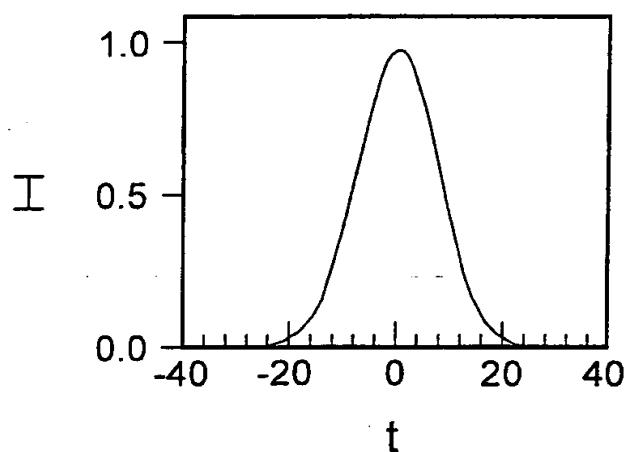
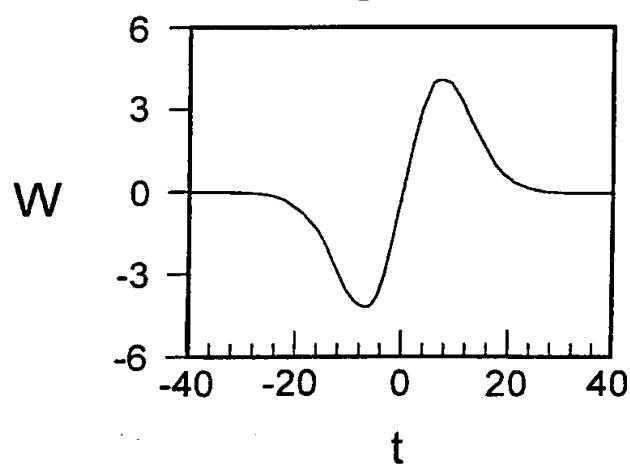
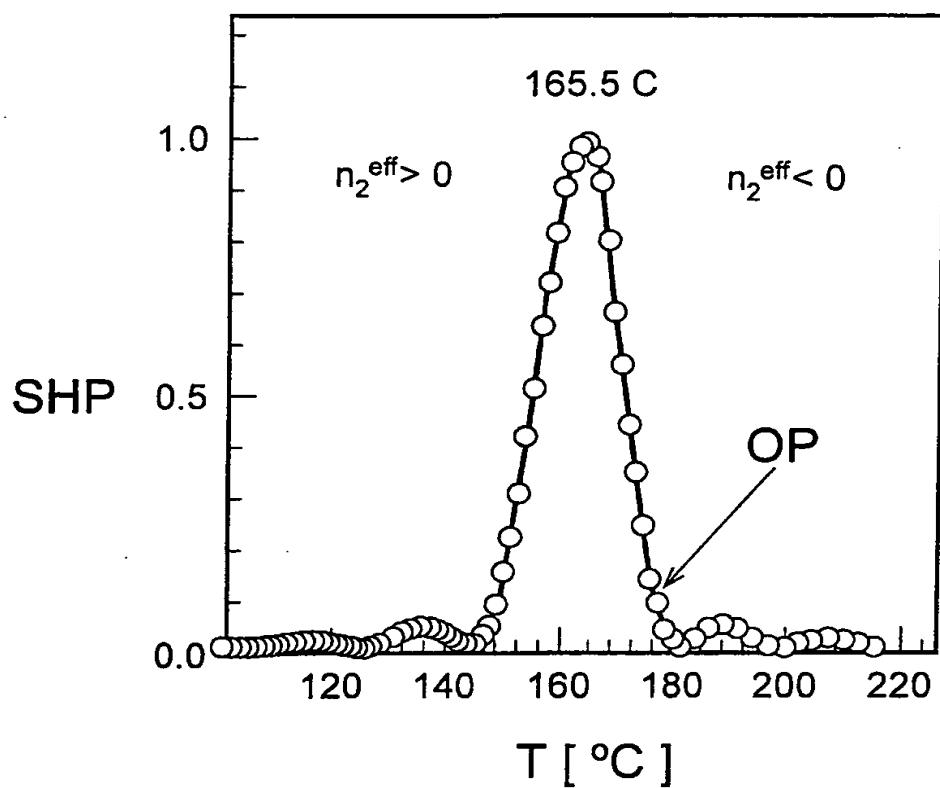


Fig. 1B



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Fig. 2



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Fig. 3

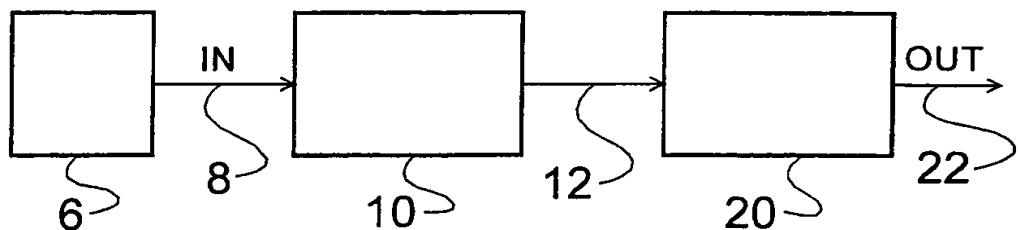


Fig. 5

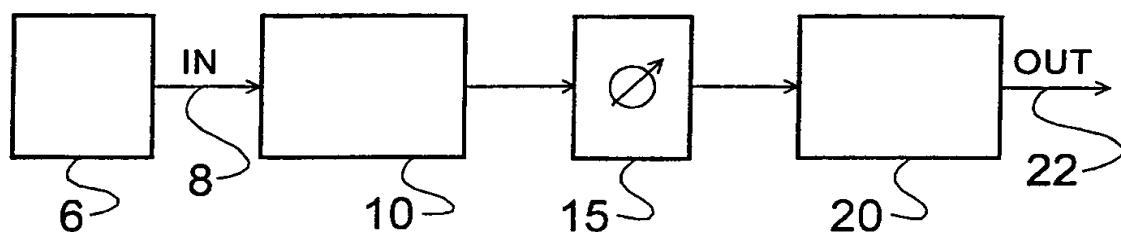
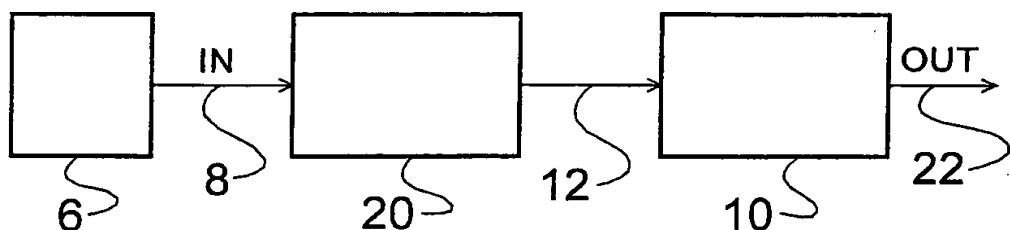


Fig. 6



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Fig. 4A

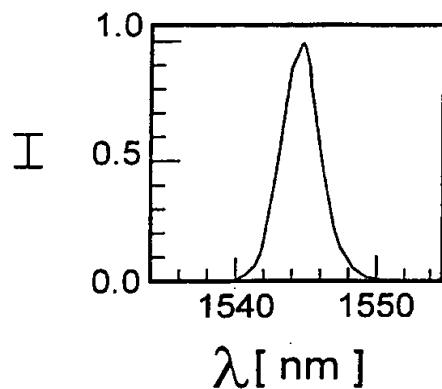


Fig. 4B

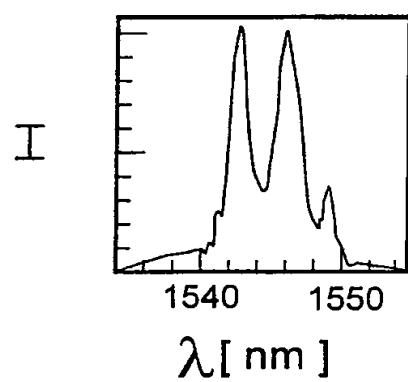
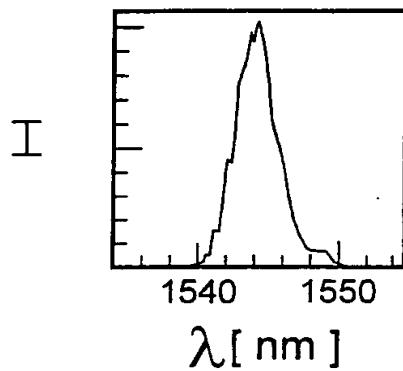
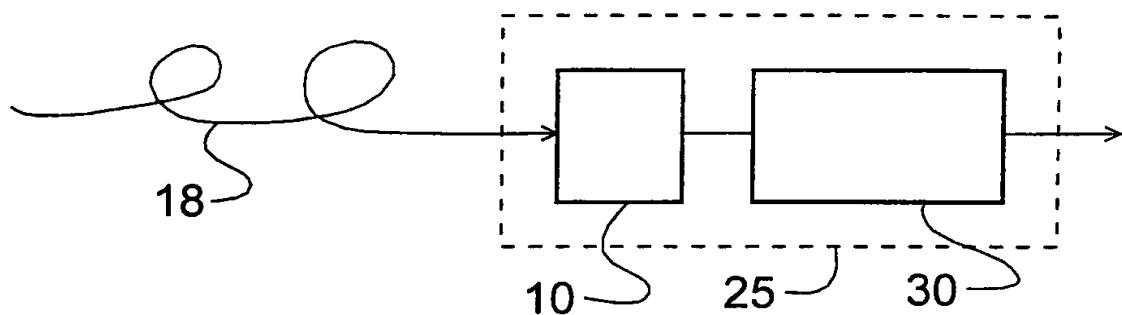


Fig. 4C



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Fig. 7



INTERNATIONAL SEARCH REPORT

International Application No
PCT/GB 00/00605

A. CLASSIFICATION OF SUBJECT MATTER IPC 7 G02F1/35 H04B10/18		
According to International Patent Classification (IPC) or to both national classification and IPC		
B. FIELDS SEARCHED Minimum documentation searched (classification system followed by classification symbols) IPC 7 G02F H04B		
Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched		
Electronic data base consulted during the international search (name of data base and, where practical, search terms used)		
C. DOCUMENTS CONSIDERED TO BE RELEVANT		
Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	<p>PARE C ET AL: "Compensating for dispersion and the nonlinear Kerr effect without phase conjugation" OPTICS LETTERS, 1 APRIL 1996, OPT. SOC. AMERICA, USA, vol. 21, no. 7, pages 459-461, XP002139461 ISSN: 0146-9592 abstract page 461, right-hand column, line 10 - line 16</p> <p>---</p> <p style="text-align: center;">-/-</p>	1-5
<input checked="" type="checkbox"/> Further documents are listed in the continuation of box C.		<input type="checkbox"/> Patent family members are listed in annex.
* Special categories of cited documents : "A" document defining the general state of the art which is not considered to be of particular relevance "E" earlier document but published on or after the international filing date "L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified) "O" document referring to an oral disclosure, use, exhibition or other means "P" document published prior to the international filing date but later than the priority date claimed		
Date of the actual completion of the international search 5 June 2000		Date of mailing of the international search report 26/06/2000
Name and mailing address of the ISA European Patent Office, P.B. 5818 Patentlaan 2 NL - 2280 HV Rijswijk Tel. (+31-70) 340-2040, Tx. 31 651 epo nl, Fax: (+31-70) 340-3016		Authorized officer Galanti, M

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International Application No
PCT/GB 00/00605

C.(Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT

Category	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	<p>PARE C ET AL: "Split compensation of dispersion and self-phase modulation in optical communication systems" OPTICS COMMUNICATIONS, 1 FEB. 1999, ELSEVIER, NETHERLANDS, vol. 160, no. 1-3, pages 130-138, XP002139462 ISSN: 0030-4018 abstract; figure 1B</p> <p>---</p>	4-19
A	<p>DESALVO R ET AL: "Self-focusing and self-defocusing by cascaded second-order effects in KTP" OPTICS LETTERS, 1 JAN. 1992, USA, vol. 17, no. 1, pages 28-30, XP002139463 ISSN: 0146-9592</p> <p>---</p>	
A	<p>VIDAKOVIC P ET AL: "Large nonlinear phase shift owing to cascaded $\chi^{(2)}$ in quasi-phase-matched bulk LiNbO_3" OPTICS LETTERS, 1 MARCH 1997, OPT. SOC. AMERICA, USA, vol. 22, no. 5, pages 277-279, XP002139464 ISSN: 0146-9592 cited in the application</p> <p>---</p>	
A	<p>SUNDHEIMER M L ET AL: "Large nonlinear phase modulation in quasi-phase-matched KTP waveguides as a result of cascaded second-order processes" OPTICS LETTERS, 1 SEPT. 1993, USA, vol. 18, no. 17, pages 1397-1399, XP002139465 ISSN: 0146-9592</p> <p>---</p>	
A	<p>FANG H ET AL: "Cascaded second-order nonlinearity in nonuniformly temperature tuned LiNbO_3 channel waveguide" CONFERENCE PROCEEDINGS. LEOS'98. 11TH ANNUAL MEETING. IEEE LASERS AND ELECTRO-OPTICS SOCIETY 1998 ANNUAL MEETING (CAT. NO. 98CH36243), CONFERENCE PROCEEDINGS. LEOS'98. 11TH ANNUAL MEETING. IEEE LASERS AND ELECTRO-OPTICS SOCIETY 1998 ANNUAL MEETING, OR, pages 61-62 vol. 2, XP002139467 1998, Piscataway, NJ, USA, IEEE, USA ISBN: 0-7803-4947-4</p> <p>---</p> <p style="text-align: center;">-/-</p>	

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PCT/GB 00/00605

C.(Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
P, X	<p>ALAM S -U ET AL: "Cascaded nonlinearity: a simple technique to compensate Kerr effect in optical amplifiers" OFC/I0OC'99. OPTICAL FIBER COMMUNICATION CONFERENCE AND THE INTERNATIONAL CONFERENCE ON INTEGRATED OPTICS AND OPTICAL FIBER COMMUNICATIONS (CAT. NO.99CH36322), OFC/I0OC'99. OPTICAL FIBER COMMUNICATION CONFERENCE AND THE INTERNATIONAL CONFERENCE ON IN, pages 5-7 vol.3, XP002139466 1999, Piscataway, NJ, USA, IEEE, USA the whole document</p> <p>-----</p>	1-19